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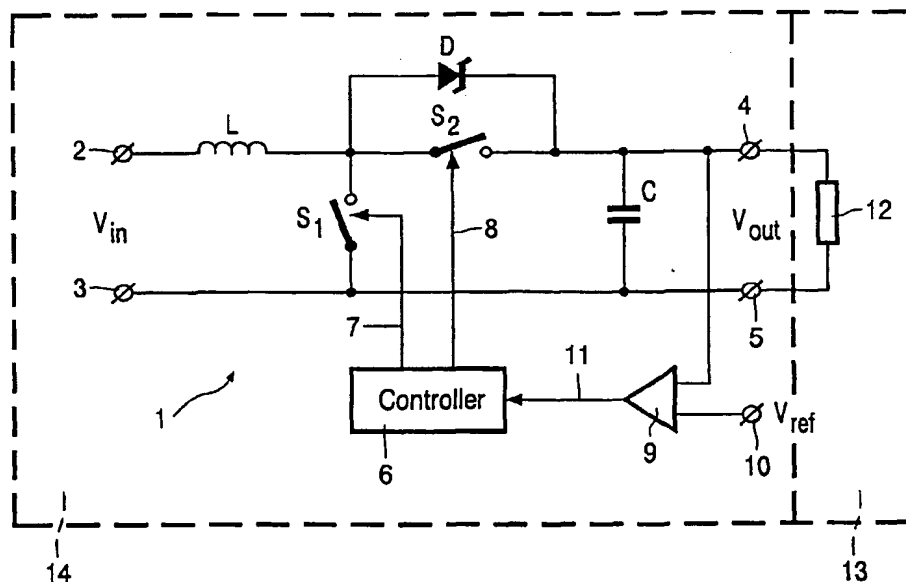
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- (71) Applicant: KONINKLIJKE PHILIPS ELECTRONICS N.V. [NL/NL]; Groenewoudseweg 1, NL-5621 BA Eindhoven (NL).
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(54) Title: A SINGLE REFERENCE DC/DC CONVERTER



(57) Abstract: A DC/DC converter (1), comprising inductive electrical energy storage means (L), switching means (S1, S2) and control means (6). The control means (6) are arranged for selectively operating the switching means (S1, S2) for transferring an amount of electrical energy from the energy storage means (L) to an output of the DC/DC converter (1), for providing a desired output voltage (Vout), in accordance with a two-state switching cycle comprising a minimum and a maximum duty cycle (Dmin, Dmax).

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A single reference DC/DC converter

The present invention relates to a DC/DC converter, comprising inductive electrical energy storage means, switching means and control means, wherein the control means are arranged for selectively operating the switching means for transferring an amount of electrical energy from the energy storage means to an output of the DC/DC converter, for  
5 providing a desired output voltage.

A DC/DC converter of this type is known from International patent application WO 95/34121 in the name of applicant.

In practice, a DC/DC converter of the above type can be operated in a continuous or PWM (Pulse Width Modulation) mode, wherein electrical energy is  
10 continuously stored in the energy storage means, or in a discontinuous or PFM (Pulse Frequency Modulation) mode, wherein the energy storage means may become completely discharged.

In a single output DC/DC converter operated in PWM mode, a typical switching cycle comprises a first phase wherein energy is stored in the energy storage means  
15 and a second phase wherein energy is transferred from the energy storage means to the output of the converter. The output power of a DC/DC converter operated in PWM mode is controlled by its duty cycle, which is the ratio of the length of the first phase and the total length of the switching cycle, i.e. the sum of the first and second phases.

For controlling the output voltage of the known DC/DC converter a voltage  
20 window is required, comprising an upper output voltage reference level and a lower output voltage reference level. Controlling the output voltage using such a voltage window, causes a random low frequency ripple in the output voltage and, of course, a spread in the output voltage. These effects can be reduced by reducing the voltage window, however this reduction is limited due to process spreading in voltage comparators used.

25 The size of the ripple is directly related to the current by which the energy storage means are charged and discharged, and relates directly to the duty cycle with which the converter is operated. A high duty cycle, implying that a relatively large amount of electrical energy is stored in the energy storage means and discharged therefrom, increases the current and thereby the output ripple, whereas a low duty cycle, implying less energy

transfer, decreases the current and, accordingly, the low frequency ripple at the output voltage. A relatively high voltage drop in the output voltage occurs during the second phase of the switching cycle, if the energy storage means are discharged with a relatively high current. When the output voltage, for control purposes, is measured during this second phase, the duty cycle and the discharge current will have a direct negative influence on the accuracy of the measurement.

It is an object of the present invention to provide a DC/DC converter of the above-mentioned type, using a single voltage reference level for controlling the output voltage, thereby reducing the dependency of the voltage measurement on the ripple voltage.

This object is solved in a DC/DC converter according to the present invention, in that the control means are configured for operatively controlling the switching means for transferring electrical energy in accordance with a two-state switching cycle comprising a minimum and a maximum duty cycle.

The present invention is based on the insight that, while the output voltage is above its desired value, set by a reference voltage, the converter is not so heavily loaded, such that during the subsequent switching cycle less energy has to be transferred to the energy storage means, thereby reducing the voltage ripple at the output voltage as disclosed above. Only, in the case that the output voltage drops below its desired value, a greater amount of electrical energy has to be stored in the energy storage means during the subsequent switching cycle, in order to restore the output voltage at its required level. As a result, the overall voltage ripple is reduced while the control means can be of a relatively simple design, using a single reference voltage and a two-state duty cycle control, providing a very stable control of the converter.

In a preferred embodiment of the invention, the DC/DC converter comprises:

- first and second input terminals for receiving an input voltage  $V_{in}$ ;
- first and second output terminals for providing an output voltage  $V_{out}$ ;
- a coil, having first and second connection ends, wherein the first connection end connects to the first input terminal;
- first switching means operatively connected to provide a conduction path from the second connection end of the coil to the second input terminal;
- second switching means operatively connected to provide a conduction path from the second connection end of the coil to the first output terminal;

- diode means, parallel connected to the second switching means, and providing a conduction path from the second connection end of the coil to the first output terminal;

- capacitor means connected between the first and second output terminals;

5 - control means arranged for operatively switching the first and second switching means into their closed or conductive state and their open or non-conductive state, and

- comparator means, configured for comparing the output voltage  $V_{out}$  with a reference voltage  $V_{ref}$  for providing a control signal to the control means for switching the switching means in accordance with the minimum and maximum duty cycle.

10 Preferably, switching means constructed as MOS (Metallic Oxide Semiconductor) transistor means are used, having their control terminal (gate) connected with the control means for controlling the conductive or non-conductive state of the transistors.

15 The DC/DC converter according to the invention is of particular advantage if applied in a portable electronic appliance, such as but not limit to battery powered appliances.

The invention will now be described in more detail with reference to the accompanying drawings showing, as an exemplary embodiment, a DC/DC up-converter, wherein:

Figure 1 shows a circuit diagram of a single output DC/DC up-converter in accordance with the present invention.

Figure 2 shows, in a graphic representation, the output voltage at the output of the DC/DC up-converter shown in figure 1.

Figure 3 shows, in a graphic representation, current flow in the inductive energy storage means in the DC/DC up-converter shown in figure 1.

Figure 4 shows, in a mode state diagram, a switching sequence in accordance with the invention for the DC/DC up-converter shown in figure 1 operated in PWM mode.

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Figure 1 shows a DC/DC up-converter 1 operated in accordance with the present invention, and having a single output.

The converter 1 comprises inductive electrical energy storage means taking the form of a coil L and first switching means S1, series connected between a first input terminal 2 and a second input terminal 3. The connection of the coil L and the first switching means S1 connects via second switching means S2 to a first output terminal 4. A diode D is parallel  
5 connected with the second switching means S2 and provides a current conductive path from the first input terminal 2 to the first output terminal 4. The second input terminal 3 and a second output terminal 5 connect through a common conductive path, for example the earth or mass of an electronic appliance. A smoothing capacitor C connects between the first and second output terminals 4, 5.

10 The converter 1 is operated to provide a controlled or regulated output voltage  $V_{out}$  at the output terminals 4, 5 in response to an input voltage  $V_{in}$  at the input terminals 2, 3. To this end, a controller or control means 6 are provided for operating the first and second switching means S1 and S2 in accordance with a switching sequence, wherein the output voltage  $V_{out}$  is higher than the input voltage  $V_{in}$ . The control of the first and second  
15 switching means S1 and S2 is schematically indicated by arrows 7, 8, respectively.

Comparator means 9 are provided, for comparing the output voltage  $V_{out}$  with a single reference voltage  $V_{ref}$  provided at an input terminal 10 of the comparator means 9. An output of the comparator means 9 connects to an input of the control means 6, as schematically indicated by arrow 11.

20 Figure 3 shows the coil current I against the time t in a typical switching cycle in a Pulse Width Modulation (PWM) conversion, wherein the current I through the coil L does not become zero. During a first phase  $\Phi 1$  energy is stored or build up in the coil L, whereas in a second phase  $\Phi 2$  of the PWM switching cycle the stored energy is delivered to the output terminals 4, 5 of the converter 1. In the first phase  $\Phi 1$ , the first switching means  
25 S1 are closed, that is in a current conductive state, while the second switching means S2 are open, that is in a non-current conductive state. During the first phase  $\Phi 1$  current flows only through the coil L storing electrical energy therein. During this phase, the current I through the coil L increases. In the second phase  $\Phi 2$  the first switching means S1 are open and the second switching means S2 are closed. In this phase, the current I through the coil drops  
30 because energy is delivered to a load 12 connected across the output terminals 4,5 of the converter 1. This results in a ripple 20 in the output voltage  $V_{out}$ , as shown in figure 2, the frequency of which equals the switching frequency of the converter 1.

The ripple 20 in the output voltage is also caused by the charging and uncharging of the output capacitor C and the current through the equivalent series resistance

(ESR) of this capacitor C. The size of the ripple 20 is directly related to the coil current I, which is controlled by the duty cycle of the converter 1.

The duty cycle D is defined as:  $D = t_1/(t_1+t_2) = t_1/T$

wherein:  $t_1$  = the length in time of the first phase  $\Phi_1$  wherein the first switching means S1 are closed;

$t_2$  = the length in time of the second phase  $\Phi_2$  wherein the second switching means S2 are closed, and

$T = t_1 + t_2$ .

In accordance with the present invention, the control means 6 are arranged for switching the first and second switching means S1 and S2 following a two-state duty cycle, having a minimum value  $D_{min}$  and a maximum value  $D_{max}$ , defined by:

$D_{max} = t_{1max}/(t_{1max} + t_{2min})$

wherein:  $t_{1max}$  = maximum length in time of  $t_1$ , and

$t_{2min}$  = minimum length in time of  $t_2$ ;

$D_{min} = t_{1min}/(t_{1min} + t_{2max})$

wherein:  $t_{1min}$  = minimum length in time of  $t_1$ , and

$t_{2max}$  = maximum length in time of  $t_2$ ,

wherein:  $T = t_{1max} + t_{2min} = t_{1min} + t_{2max}$ .

As shown in figure 2, the output voltage  $V_{out}$  is measured at sample moments at the end of a conversion cycle ( $t=T$ ), as indicated by arrows 15, 16, 17, 18, 19. In accordance with the present invention, if at a sample moment the output voltage  $V_{out}$  is above the reference level  $V_{ref}$ , such as at the sample moments 15 and 18, the subsequent switching cycle will have the minimum duty cycle  $D_{min}$ . If the output voltage  $V_{out}$ , at the sample moment, drops below the reference voltage  $V_{ref}$ , such as indicated at the sample moments 16, 17 and 19, the subsequent switching cycle will have the maximum duty cycle  $D_{max}$ .

Accordingly, by controlling the switching means in accordance with the present invention in a two-state cycle, a single reference level  $V_{ref}$  can be applied for controlling the output voltage  $V_{out}$ .

Figure 4 shows a state diagram illustrating the operation of the single reference DC/DC converter control means 6 in accordance with the present invention.

Starting from state  $\Phi_1$  of the maximum duty cycle  $D_{max}$ , then if the time  $t$  during a cycle is above  $t_{1max}$ , the switching means S1 and S2 are switched to state  $\Phi_2$  of the conversion cycle with maximum duty cycle, i.e. state  $\Phi_2$ ,  $D_{max}$  in the diagram. If at the end

of the duty cycle, i.e.  $t > T$  the output voltage  $V_{out}$  is less than the reference voltage  $V_{ref}$ , i.e.  $V_{out} < V_{ref}$ , the control means 6 remain in the conversion cycle with maximum duty cycle  $D_{max}$ .

5 Likewise, if the control means 6 operate in a conversion cycle with minimum duty cycle, i.e. state  $\Phi 1$ ,  $D_{min}$  and if  $t > t_{1min}$ , the switching means  $S1$  and  $S2$  are switched into state  $\Phi 2$ , wherein energy is transferred to the output of the converter 1. At the end of the duty cycle, i.e.  $t > T$  and if  $V_{out} > V_{ref}$ , the converter remains in its conversion cycle with minimum duty cycle  $D_{min}$ .

10 If the output voltage  $V_{out} < V_{ref}$  at the end of a conversion cycle, i.e.  $t > T$ , then the control means will switch from the state  $\Phi 2$  with minimum duty cycle  $D_{min}$  to the state  $\Phi 1$  of the conversion cycle with maximum duty cycle  $D_{max}$ . On the other hand, if  $t > T$  and  $V_{out} > V_{ref}$ , the control means 6 will change from the state  $\Phi 2$  of the conversion cycle with maximum duty cycle  $D_{max}$  to the state  $\Phi 1$  of the conversion cycle with minimum duty cycle  
15  $D_{min}$ .

In the DC/DC up-converter shown in figure 1, the second switching means  $S2$  are optional, and are used to increase the power conversion efficiency of the DC/DC converter 1.

20 The DC/DC converter operating in accordance with the principles of the present invention may be used with or in an electronic appliance, such as a portable electronic appliance 13, or arranged to form a separate power supply 14, both schematically indicated by dashed lines in figure 1.



## CLAIMS:

1. A DC/DC converter (1), comprising inductive electrical energy storage means (L), switching means (S1, S2) and control means (6), wherein said control means (6) are arranged for selectively operating said switching means (S1, S2) for transferring an amount of electrical energy from said energy storage means (L) to an output of said DC/DC converter (1), for providing a desired output voltage (Vout), characterized in that said control means (6) are configured for operatively controlling said switching means (S1, S2) for transferring electrical energy in accordance with a two-state switching cycle comprising a minimum and a maximum duty cycle (Dmin, Dmax).
2. A DC/DC converter (1) according to claim 1, wherein said control means (6) are arranged for comparing said output voltage (Vout) with a reference voltage (Vref), and wherein said switching means (S1, S2) are controlled such that if said output voltage (Vout) is below said reference voltage (Vref), the maximum duty cycle (Dmax) is used for the next switching cycle, and if said output voltage (Vout) is higher than said reference voltage (Vref) the minimum duty cycle (Dmin) is used for the next switching cycle.
3. A DC/DC converter (1) according to claim 1 or 2, wherein said control means (6) are arranged for controlling said output voltage (Vout) in a Pulse Width Modulation (PWM) mode switching cycle.
4. A DC/DC converter (1) according to any of the previous claims, comprising:
  - first and second input terminals (2, 3) for receiving an input voltage Vin;
  - first and second output terminals (4, 5) for providing an output voltage Vout;
  - a coil (L), having first and second connection ends, wherein said first connection end connects to said first input terminal (2);

- first switching means (S1) operatively connected to provide a conduction path from said second connection end of said coil (L) to said second input terminal (3);
- second switching means (S2) operatively connected to provide a conduction path from said second connection end of said
- 5 coil (L) to said first output terminal (4);
- diode means (D) parallel connected to said second switching means (S2), and providing a conduction path from said second connection end of said coil (L) to said first output terminal (4);
- capacitor means (C) connected between said first and second output
- 10 terminals (4, 5);
- control means (6) arranged for operatively switching said first and second switching means (S1, S2) into their closed or conductive state and their open or non-conductive state, and
- comparator means (9), configured for comparing said output voltage (Vout)
- 15 with a reference voltage (Vref) for providing a control signal to said control means (6) for switching said switching means (S1, S2) in accordance with said minimum and maximum duty cycle (Dmin, Dmax).

5. A DC/DC converter (1) according to claim 2, 3 or 4, wherein said switching  
20 means (S1, S2) comprise semiconductor switching means, in particular MOS (Metallic Oxide Semiconductor) transistor means.

6. A DC/DC converter (1) according to any of the previous claims, wherein said  
25 control means (6) are configured for operating in an up-conversion mode providing an output voltage (Vout) at its output terminals (4, 5) which is higher than an input voltage (Vin) at its input terminals (2, 3).

7. A power supply (14) comprising a DC/DC converter (1) according to any of  
the previous claims.

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8. A portable electronic appliance (13) comprising a DC/DC converter (1)  
according to any of the previous claims.

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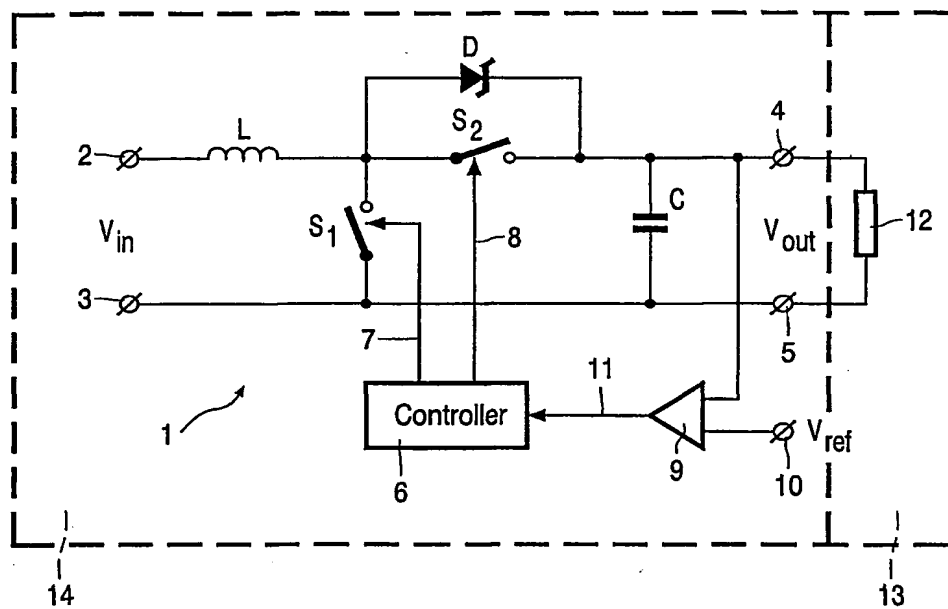


FIG. 1

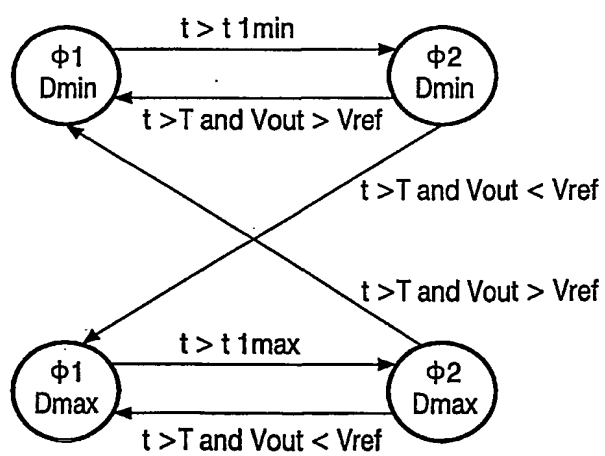


FIG. 4

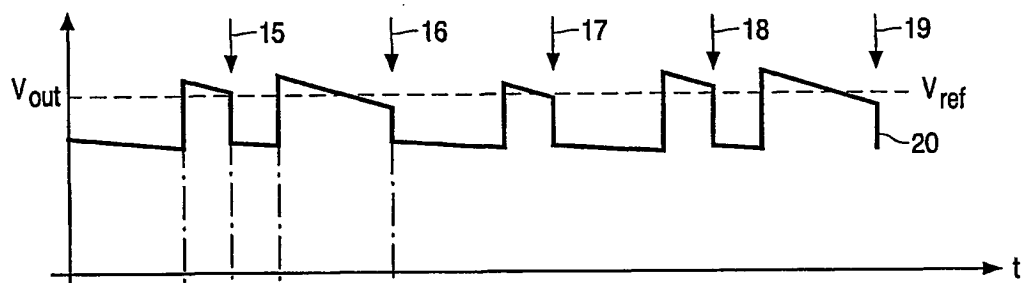


FIG. 2

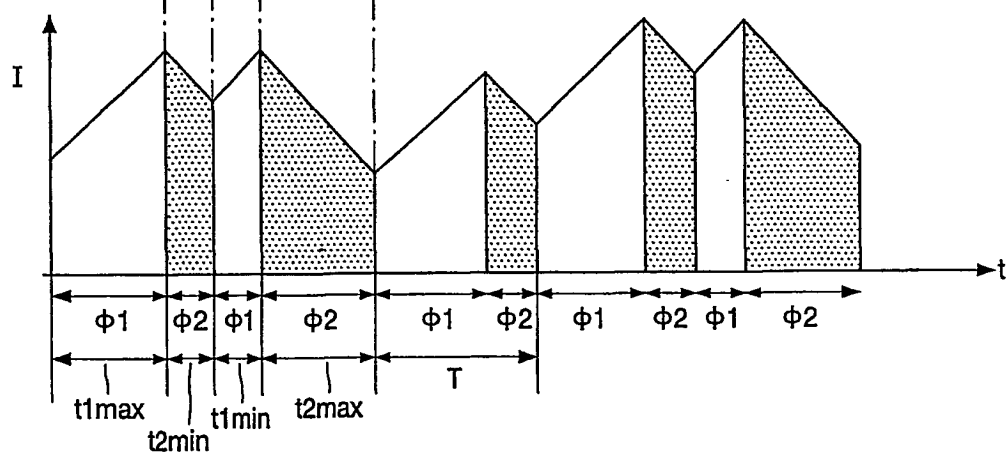


FIG. 3

# INTERNATIONAL SEARCH REPORT

International Application No  
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A. CLASSIFICATION OF SUBJECT MATTER  
IPC 7 H02M3/156 H02M3/157

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7 H02M

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

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**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

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X	PATENT ABSTRACTS OF JAPAN vol. 011, no. 187 (E-516), 16 June 1987 (1987-06-16) & JP 62 016068 A (MATSUSHITA ELECTRIC), 24 January 1987 (1987-01-24) abstract	1-8
X	WO 98 44622 A (KONINKLIJKE PHILIPS ELECTRONICS) 8 October 1998 (1998-10-08) the whole document	1-8
X	US 5 625 279 A (HUSTON W. RICE ET AL.) 29 April 1997 (1997-04-29) figure 1 column 1, line 50 - line 62	1-8
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## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 914 865 A (GEORGE BARBEHENN ET AL.) 22 June 1999 (1999-06-22) abstract figures 1-3 column 1, line 61 -column 2, line 32	1-8
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Information on patent family members

International Application No

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